Appl. Ser. No.: 10/789,756 Atty. Docket No.: 30210-102CIP

Reply to Office Action dtd. 09 September 2005

## Amendments to the Specification

Please substitute the following paragraph for the paragraph [0015] currently pending in the application:

Figure 3 schematically illustrates a single-strap embodiment of a RF cup-coil 2, wherein an arcuate strap 10 is connected to a base ring 12 and passes through an imaginary central axis 18 of the base ring 12. As noted above, the term "arcuate" is meant to encompass nonhemispherical shapes such as, for example, rectangles, ellipses, parabolas, or other shapes. Strap 10 is directly connected to base ring 12 at one end at point C 20, and electrically connected to base ring 12 through tuning capacitors C<sub>MA</sub>, C<sub>MB</sub> 14 bridging the gaps 26 between its other end (point D 22) and two segments including component points A 17 and B 19, respectively, of base ring 12. The strap 10 and base ring 12 can be implemented with microstrip conductor lines (e.g., copper) or any other conducting material, and are dimensioned so as to receive the anatomical region of interest (e.g., a human breast.) The capacitors CA, CB, CC 16 and the inherent inductances L<sub>4A</sub>, L<sub>2B</sub>, L<sub>3C</sub> of the segments of microstrip lines form a resonance system that can be tuned to a particular resonance frequency based on the requirement of the main magnet system of the magnetic resonance (MR) instrument. In order to tune the cup-coil 2 efficiently, fixed and tunable capacitors CA, CB, CC 16 are deployed at strategically selected cuts 24 in the microstrip segments comprising strap 10 and base ring 12. The selection and adjustment of tuning capacitors C<sub>MA</sub>, C<sub>MB</sub> 14 is based upon the resonance requirement of the cup-coil at a desired frequency. For instance, the capacitors C<sub>MA</sub>, C<sub>MB</sub> 14 can be adjusted such that a resonance frequency of 63.87MHz is achieved, consistent with a 1.5T main magnetic field of a MR system for proton imaging. Other magnetic field strengths can be implemented, such as 3T and higher. Capacitors CA, CB, CC 16 can be selected and/or adjusted such that their reactances compensate the inherent inductive reactances of the cup coil the cup-coil 2, and such that together with the microstrip inductances L<sub>4A</sub>, L<sub>2B</sub>, L<sub>3C</sub>, the desired resonance frequency is obtained. They also reduce eddy currents that would result as a consequence of the switching gradients of the MR system. The reactance associated with capacitor  $C_{\frac{3C}{2}}$  should be chosen such that it compensates for the inductance associated the inductance  $L_{3\underline{C}}$  of the upper strap.

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Please substitute the following paragraph for the paragraph [0016] currently pending in the application:

Figures 4A and 4B illustrate, respectively, the two modes (Mode<sub>0</sub>, Mode<sub>1</sub>) of operation available in the single-strap RF cup-coil 2 and the magnetic fields associated therewith. In Mode<sub>0</sub>, no current flows through strap 10 while a current I 26 induced in the base ring 12 by the magnetic flux density travels around the annular base ring 12 along current path A-C-B-D. In Mode<sub>1</sub>, a 90° phase shifted current 2I 30 is induced in the strap 10 and is divided symmetrically into two currents I 32 between two halves of the base ring 12 (or vice versa) along current paths D-A-C and D-B-C respectively. Figures 4A and 4B include Cartesian xyz-space axes that help illustrate how the superposition of the modes establishes a rotating magnetic field phasor B<sub>RF</sub> 6 (shown in Figure 4C) orthogonal to the uniform static uniform field B<sub>0</sub> 8 (shown in Figure 2) of the MR instrument.

Please substitute the following text for the text in paragraph [0018] currently pending in the application up to the sentence beginning "Specifically, the resonance...":

Figure 6A presents an electronic equivalent circuit 40 of the single-strap RF cup coil 2 depicted in Figure 3. Nodes A-D in circuit 40 correspond to the identically labeled points in the schematic model of the cup-coil 2 shown in Figure 3. Electrical losses in the cup-coil 2 are represented in the model circuit by resistors R<sub>1A</sub>, R<sub>B</sub> and R<sub>C</sub> through R<sub>3</sub>. In circuit 40, capacitors C<sub>A</sub>, C<sub>B</sub>, C<sub>C</sub> represent the fixed and tunable capacitors 16 described above, inductances L<sub>A</sub>, L<sub>B</sub>, L<sub>C</sub> represent the inherent inductances of the segments of the microstrip lines, and C<sub>MA</sub> and C<sub>MB</sub> represent the tuning capacitors 14 bridging the gaps between the arcuate conductor and two segments of the base ring conductor. The operational and dimensional specifications of a single-strap RF cup-coil implemented using standard fixed and variable capacitors on a dielectric "former" are reflected in Figure 6B, wherein the reference characters correspond to the tuning capacitors, fixed and tunable capacitors and component points described above, and in Table One and Table Two.